



A variable probe pitch micro-Hall effect method

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Abstract

Hall effect metrology is important for a detailed characterization of the electronic properties of new materials for nanoscale electronics. The micro-Hall effect (MHE) method, based on micro four-point probes, enables a fast characterization of ultrathin films with minimal sample preparation. Here, we study in detail how the analysis of raw measurement data affects the accuracy of extracted key sample parameters, i.e., how the standard deviation on sheet resistance, carrier mobility and Hall sheet carrier density is affected by the data analysis used. We compare two methods, based primarily on either the sheet resistance signals or the Hall resistance signals, by theoretically analysing the effects of electrode position errors and electrical noise on the standard deviations. We verify the findings with a set of experimental data measured on an ultrashallow junction silicon sample. We find that in presence of significant electrical noise, lower standard deviation is always obtained when the geometrical analysis is based on the sheet resistance signals. The situation is more complicated when electrode position errors are dominant; in that case, the better method depends on the experimental conditions, i.e., the distance between the insulating boundary and the electrodes. Improvement to the accuracy of Hall Effect measurement results is crucial for nanoscale metrology, since surface scattering often leads to low carrier mobility.

Introduction

Materials characterization becomes increasingly difficult as the dimensions of transistors continue to decrease. Although three dimensional electrical characterization is the ultimate goal of materials characterization, conventional metrology for thin-film characterization still plays an important role in development of materials used in nanoelectronics [1]. Hall effect measurements

have been employed for decades to electrically characterize samples and extract important metrics, such as concentration, mobility and type of charge carriers [2,3]. Some of the measurement methods require significant sample preparation while other methods are destructive [2]. Great progress in measurement simplicity and accuracy has been achieved with the intro-

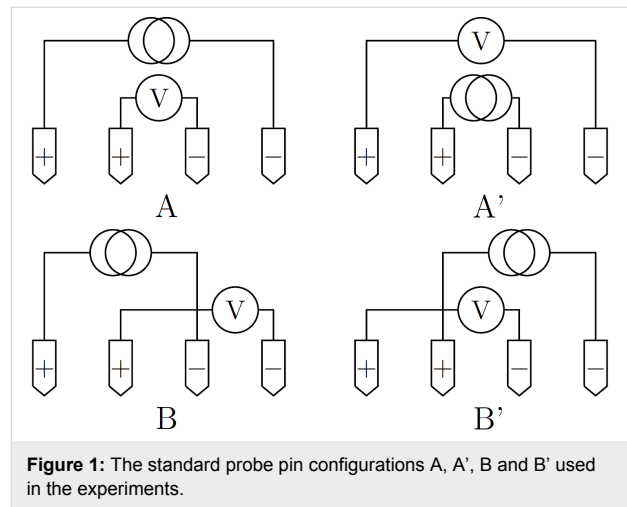
duction of the micro-Hall effect (MHE) method [4]. The MHE measurement itself is performed simply by placing a micro four-point probe (M4PP) in parallel and close proximity to an insulating boundary, with an orthogonal magnetic field applied. Then the measured resistance will have three contributions: a drift term, a Hall effect term and a magnetoresistive term. In a comparative study by Clarysse et al., the MHE method has been shown to have higher accuracy than more conventional setups using square van der Pauw geometries [5]. Van der Pauw geometries often suffer from inaccurate contact placement, which easily results in measurement errors of a few percent [6]. Comparing the MHE method with measurements performed using a cloverleaf, Petersen et al. [7] have shown a 1:1 correlation between the measurements. Cloverleaf measurements are, however, challenging because of the sample definition required before any actual measurements can be performed. Hence, the MHE method holds several advantages over other well-known techniques, even though low-mobility samples can also be characterized by the latter [8].

The key to accurate extraction of sheet resistance R_0 , Hall sheet carrier density N_{HS} and Hall mobility μ_{H} from MHE measurements is to determine the exact distance between the probe and the insulating boundary. To this end, different measurement strategies have been described using micro four-point probes [4,9–11]. Most recently, a strategy based on variable probe pitch measurements using a multi-point probe with different subsets of four electrodes has been developed [11,12]. Similar strategies using variable probe pitch multi-point probes have been used for other systems, including current-in-plane tunneling measurements [13], junction-leakage measurements [14] and surface-conductivity measurements of bulk materials [15,16].

In this study, we present the variable probe pitch MHE method applied to an equidistant micro seven-point probe (M7PP), and compare two independent ways of extracting the relevant sample parameters from the same set of measurements. Furthermore, we will demonstrate the sensitivity of each method to position errors, as well as to electrical noise. Finally, we will present measurements on a B-doped Si ultrashallow junction, supporting our findings.

Micro-Hall Effect Theory

The fundamentals of Hall Effect measurements with a collinear M4PP have previously been described in detail [4]. However, we will briefly outline some of the most important characteristics here. For any four-point probe, 6 non-trivial configurations of current and electrode pins can be measured, but for this work, only the configuration pairs (A, A') and (B, B'), illustrated in Figure 1, are relevant.



Crucial in understanding MHE measurements are the definitions of the resistance difference for the pairs, $\Delta R_{XX'} \equiv R_X - R_{X'}$, as well as their resistance average, $\overline{R_{XX'}} \equiv (R_X + R_{X'}) / 2$, where $X \in \{A, B\}$. For an equidistant four-point probe placed parallel to an insulating boundary, the resistance difference for the (B, B') pair is

$$\Delta R_{BB'} = \frac{2R_H}{\pi} \left(3 \arctan \frac{s}{2y_0} - \arctan \frac{3s}{2y_0} \right), \quad (1)$$

where R_H is the Hall sheet resistance, s is the electrode pitch and y_0 the distance between the probe and the insulating boundary. Note that in the relevant case where the probe is placed parallel to a straight insulating boundary, the resistance difference for the (A, A') pair is $\Delta R_{AA'} = 0$. The resistance averages in the configuration pairs (A, A') and (B, B') are

$$\overline{R_{AA'}} = \mathcal{A}_+ \ln 4 + \mathcal{A}_- \ln \frac{4 + 4(y_0/s)^2}{1 + 4(y_0/s)^2}, \quad (2)$$

$$\overline{R_{BB'}} = \mathcal{A}_+ \ln 3 + \mathcal{A}_- \ln \sqrt{\frac{9 + 4(y_0/s)^2}{1 + 4(y_0/s)^2}}, \quad (3)$$

respectively, where the coefficients are given by

$$\begin{aligned} \mathcal{A}_+ &\equiv \frac{R_0}{2\pi} \left(1 + \frac{R_H^2}{R_0^2} \right), \\ \mathcal{A}_- &\equiv \frac{R_0}{2\pi} \left(1 - \frac{R_H^2}{R_0^2} \right), \end{aligned} \quad (4)$$

in which R_0 denotes the sheet resistance. It has been shown that by introducing a pseudo sheet resistance R_p , the effect of electrode position errors can be mitigated [9]. The pseudo sheet resistance is defined as the solution to the modified van der Pauw equation [17–20]

$$\exp \frac{2\pi \overline{R_{AA'}}}{R_p} - \exp \frac{2\pi \overline{R_{BB'}}}{R_p} = 1, \quad (5)$$

which will be utilized in the next section, in which the variable probe pitch method is presented in full.

Variable Probe Pitch Method

The variable probe pitch method uses measurements at different relative distances to the boundary of a sample by multiplexing several sets of four electrodes on a M7PP. These sets are called sub-probes and can be chosen with different electrode pitch. In this case, three equidistant sub-probes are used and named with reference to the index number of the four electrodes constituting the sub-probe, “1357” (20 μm pitch), “1234” and “4567” (10 μm pitch). The three sub-probes are outlined in Figure 2. Once resistance measurements have been performed in the A, A', B and B' configurations for the three sub-probes, two different ways of determining the distance to the boundary and ultimately obtaining the desired parameters, can be employed. The first method utilizes the Hall signal and will be referred to as the “Hall signal method”. The second method uses the resistance signal and will be referred to as the “resistance signal method”.

To determine the distance to the boundary, y_0 , the first step in the Hall signal method is to exploit the fact that the Hall signal decreases with distance to the boundary relative to the probe pitch, as shown in Figure 3. In other words, it is possible to uniquely determine y_0 by taking the ratio of two Hall signals ($\langle \Delta R_{BB'1} \rangle$ and $\Delta R_{BB'2}$) measured while using sub-probes with

different pitches s_1 and s_2 , i.e., by using the Hall signal $\Delta R_{BB'2}$ from the large probe, 1357, and the average of the Hall signals $\langle \Delta R_{BB'1} \rangle$ from the smaller probes, 1234 and 4567,

$$\frac{\Delta R_{BB'2}}{\langle \Delta R_{BB'1} \rangle} = \frac{f(y_0/s_2)}{f(y_0/s_1)}, \quad (6)$$

where $f(\cdot)$ is a geometrical function obtained from Equation 1.

To calculate y_0 in the resistance signal method, dual-configuration position correction is utilized, by inserting the measured

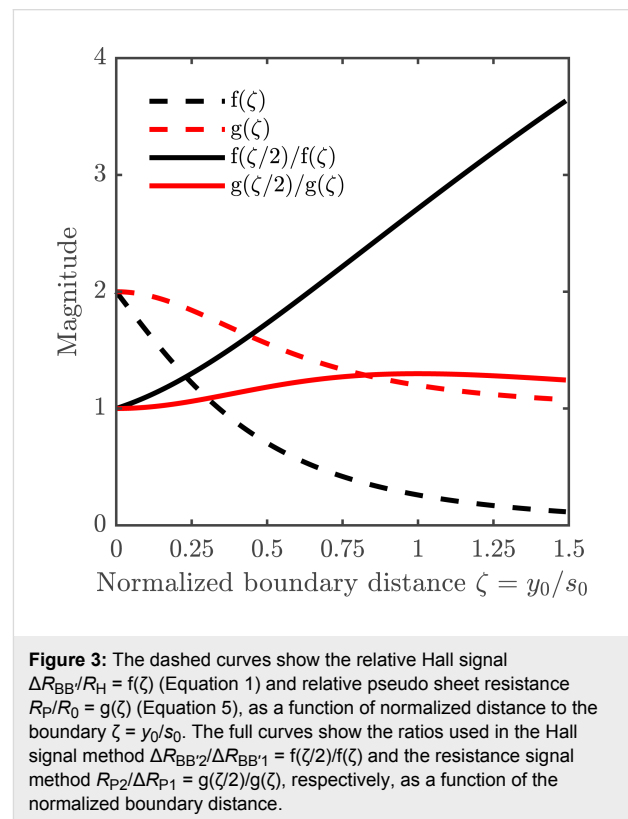


Figure 2: The three sub-probes on an M7PP used for multiplexing during measurements; a) 1357 (20 μm pitch), b) 1234 and c) 4567 (10 μm pitch). The electrode pins used in a given sub-probe are marked with green. The sample itself is highlighted in blue. The direction of magnetic flux density B_z , which is pointing into the sample, is also indicated.

resistance averages for each sub-probe in the van der Pauw equation (Equation 5). From this equation, the pseudo sheet resistance is extracted, which, due to the presence of the boundary, differs from the true sheet resistance, R_0 . By measuring the pseudo sheet resistances, $\langle R_{P1} \rangle$ and R_{P2} , at different relative distances to the boundary, using differently pitched (s_1 , s_2) sub-probes, i.e., by using the resistance signal R_{P2} from the large probe, 1357, and the average of the resistance signals $\langle R_{P1} \rangle$ from the smaller probes, 1234 and 4567, it is possible to determine y_0 from

$$\frac{R_{P2}}{\langle R_{P1} \rangle} = \frac{g(y_0/s_2)}{g(y_0/s_1)}, \quad (7)$$

where $g(\cdot)$ is a geometrical function, implicitly found from Equation 2, Equation 3 and Equation 5.

Equation 6 and Equation 7 are plotted in Figure 3 for the specific case of a probe having the reference pitch s_0 for the two smallest sub-probes and $2s_0$ for the larger sub-probe. They are plotted as a function of the normalized boundary distance $\zeta = y_0/s_0$. We introduce s_0 and ζ here to emphasize the nature and relationship between the sub-probes used in this paper; the pitches s_1 and s_2 utilized in this section are more general in nature and could also be used to describe other symmetric multipoint-probes.

After y_0 has been calculated using either method, the Hall sheet resistance R_H and the sheet resistance R_0 can be determined by means of

$$R_H = \Delta R_{BBi} / f(y_0/s_i), \quad (8)$$

$$R_0 = R_{Pi} / g(y_0/s_i), \quad (9)$$

respectively, with $i \in [1, 2]$. Finally, the Hall sheet carrier density, N_{HS} , and the Hall mobility, μ_H , can be found from [4]

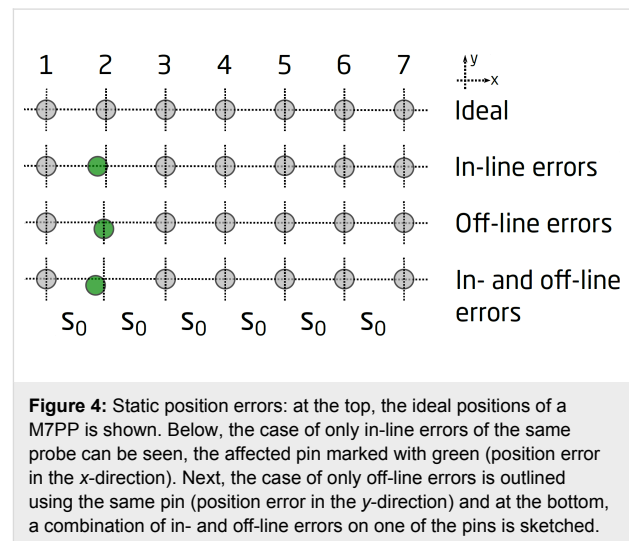
$$N_{HS} = \frac{B_z}{ZeR_H}, \quad (10)$$

and

$$\mu_H = \frac{ZR_H}{R_0 B_z}, \quad (11)$$

where Z is the sign of the charge carrier and e is the elementary charge.

The choice of using seven equidistant electrodes for the probe was carefully made, in order to minimize the contribution of in-line geometrical errors to the measured quantities, $\Delta R_{BB'}$ and R_p . The definitions of in-line and off-line geometrical errors of an M7PP are illustrated in Figure 4. Any in-line errors on pins 1 and 7 will influence the size of the large sub-probe and the average size of the small sub-probes, which explains the correlation between values measured with sub-probe 1357, and the average values obtained with sub-probes 1234 and 4567. Furthermore, an in-line error on pin 4 would be inconsequential, as the pin is shared by the two $10 \mu\text{m}$ sub-probes. Such an error will cause an increase in the measured quantity of one sub-probe, whereas a decrease in the measured quantity will result from the other, leaving the average value unchanged. Hence, it should be possible to eliminate the correlated in-line errors on pins 1, 4 and 7, while in-line errors on pins 2, 3, 5 and 6 have low or zero influence on the measured quantities R_p and $\Delta R_{BB'}$. Off-line position errors can result in complex errors that are correlated to some extent, but these are beyond the scope of this study. Electrical noise will produce uncorrelated errors on the measurements, which cannot be corrected.



The sensitivity of the resistance signal method and the Hall signal method to position errors, as well as electrical noise, will be studied in the next section, to investigate which of the two independent methods perform best, and under which circumstances.

Results and Discussion

In this section, we will evaluate numerically the expected measurement precision of the Hall signal method and the resistance signal method. The two main sources of error are geometrical errors and electrical noise, which we initially will discuss separately.

In the evaluation of geometrical errors, we will only consider mutually independent and normally distributed static position errors, meaning that if a position error is present on one of the electrode pins, this error will not change during a measurement. The relative standard deviation due to position errors, $\sigma_{\beta}^{\text{rel,pos}}$, for a given property $\beta \in \{R_0, \mu_H, N_{\text{HS}}\}$ can be calculated from

$$\begin{aligned}\sigma_{\beta}^{\text{rel,pos}} &= \frac{1}{\beta} \sqrt{\sum_{n=1}^7 \left[\left(\frac{\partial \beta}{\partial x_n} \sigma_x \right)^2 + \left(\frac{\partial \beta}{\partial y_n} \sigma_y \right)^2 \right]} \\ &\approx \sqrt{\sum_{n=1}^7 \left[\left(\frac{s_0}{\beta} \frac{\partial \beta}{\partial x_n} \right)^2 + \left(\frac{s_0}{\beta} \frac{\partial \beta}{\partial y_n} \right)^2 \right]} \cdot \frac{\sigma_{\text{pos}}}{s_0} \quad (12) \\ &= S_{\beta}^{\text{pos}} \frac{\sigma_{\text{pos}}}{s_0},\end{aligned}$$

where we have normalized to the reference pitch s_0 . The standard deviations of in-line and off-line electrode position errors are assumed to be identical, $\sigma_{\text{pos}} = \sigma_x = \sigma_y$. The symbols x_n and y_n are the x - and y -positions, respectively, of the n -th electrode pin. S_{β}^{pos} is the effective sensitivity of a given parameter to the relative position errors. This effective sensitivity is evaluated numerically for each parameter β and plotted in Figure 5, for both methods. The results generally predict an increased error with increasing distance from the boundary. The largest error is found for N_{HS} and the lowest for R_0 . Interestingly, the error of μ_H is lower than that of N_{HS} , indicating a correlation of the errors of R_0 and R_H . This effect has previously been observed experimentally [9]. For the sheet resistance, the resistance signal method has the lowest relative standard deviation up to a distance of $y_0 = 0.53s_0$ away from the boundary, beyond which point a higher precision can be obtained using the Hall signal method. The same tendencies are displayed for the Hall mobility and the Hall sheet carrier density for which the method of highest accuracy changes at $y_0 = 0.41s_0$ and $y_0 = 0.45s_0$, respectively. The superiority of the resistance signal method closer to the boundary stems from the high precision on the pseudo sheet resistance ratio (Equation 7). For longer boundary distances, the pseudo sheet resistance ratio ceases to increase with boundary distance and finally starts declining as shown in Figure 3 and thus this ratio becomes less accurate for determining the boundary distance at larger distances. Since the resistance difference ratio (Equation 6) continues to increase with boundary distance, it becomes more suitable for determining the boundary distance and subsequently R_0 , N_{HS} and μ_H at larger boundary distances. Figure 3 also shows that the resistance signal method does not result in a unique solution for the boundary distance at larger boundary distances. Thus, it is necessary to place the probe within a distance of approximately $y_0 < s_0$ from the boundary.

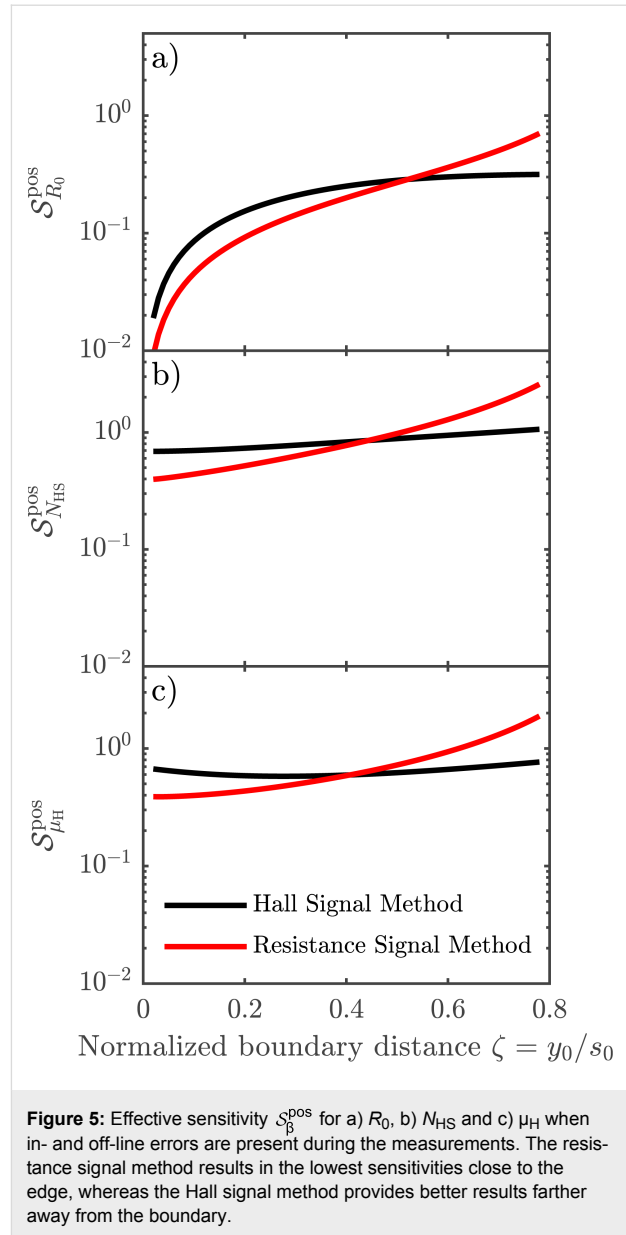


Figure 5: Effective sensitivity S_{β}^{pos} for a) R_0 , b) N_{HS} and c) μ_H when in- and off-line errors are present during the measurements. The resistance signal method results in the lowest sensitivities close to the edge, whereas the Hall signal method provides better results farther away from the boundary.

To evaluate the contribution of electrical noise to MHE measurements, we consider twelve resistance measurements (R_m , $m \in [1, 2, \dots, 12]$), i.e., four configurations for each sub-probe, in which a random voltage noise is present. The voltage noise comprises, e.g., Johnson noise from the two-point resistance and wiring resistance, as well as noise from the measurement electronics. The voltage noise is assumed to have the same standard deviation $\sigma_v = 60$ nV for all twelve resistance measurements [21], which in turn are assumed to be uncorrelated. The voltage noise causes a noise in the resistance measurements with the standard deviation $\sigma_{R_m} = \sigma_v / I$, where I is the measurement current. From the twelve configurations measured, the parameter β is calculated, and thus the relative standard deviation on β due to electrical noise is

$$\begin{aligned}\sigma_{\beta}^{\text{rel,el}} &= \frac{1}{\beta} \sqrt{\sum_{m=1}^{12} \left(\frac{\partial \beta}{\partial R_m} \sigma_{R_m} \right)^2} \\ &= \sqrt{\sum_{m=1}^{12} \left(\frac{R_0}{\beta} \frac{\partial \beta}{\partial R_m} \right)^2} \cdot \frac{\sigma_v}{IR_0} \\ &= S_{\beta}^{\text{el}} \frac{\sigma_v}{IR_0},\end{aligned}\quad (13)$$

where S_{β}^{el} is a dimensionless sensitivity of β to electrical noise. This effective sensitivity has been calculated numerically for the sheet resistance, Hall mobility and Hall sheet carrier density, while choosing the ratio $R_H/R_0 = 3:1000$ to represent the experiments, and the ratio $R_H/R_0 = 1:100$ for comparison. These results are shown in Figure 6a–c and Figure 6d–f, respectively, for both methods. There are two main mechanisms describing the results shown in Figure 6: (1) the accuracy with which the distance to the boundary is determined and (2) how the position

uncertainty translates into an error in the calculation of R_H and R_0 .

Figure 7 generalizes the results from Figure 6 in the sense that the sensitivity of each parameter to electrical noise is investigated for varying R_H/R_0 ratios. A small R_H/R_0 ratio corresponds to a low mobility sample or a setup using a small magnetic field, whereas a higher ratio indicates the opposite. We have chosen to investigate R_H/R_0 ratios from 3×10^{-3} to 1×10^{-1} , because of the nature of Equation 13, which takes into account only errors of first order. Investigating R_H/R_0 ratios below 3×10^{-3} would produce cases where the electrical noise we apply is comparable to or greater than the Hall signal, in which case Equation 13 is no longer valid. The probe is placed at a distance of $y_0 = 0.4s_0$ away from the insulating boundary, as it is most commonly done in experiments. Consider then the parameters R_0 , μ_H and N_{HS} , as produced by the Hall signal method, and outlined in Figure 7a–c using black lines. In all three cases, we observe a similar relative decrease of S_{β}^{el} with increasing

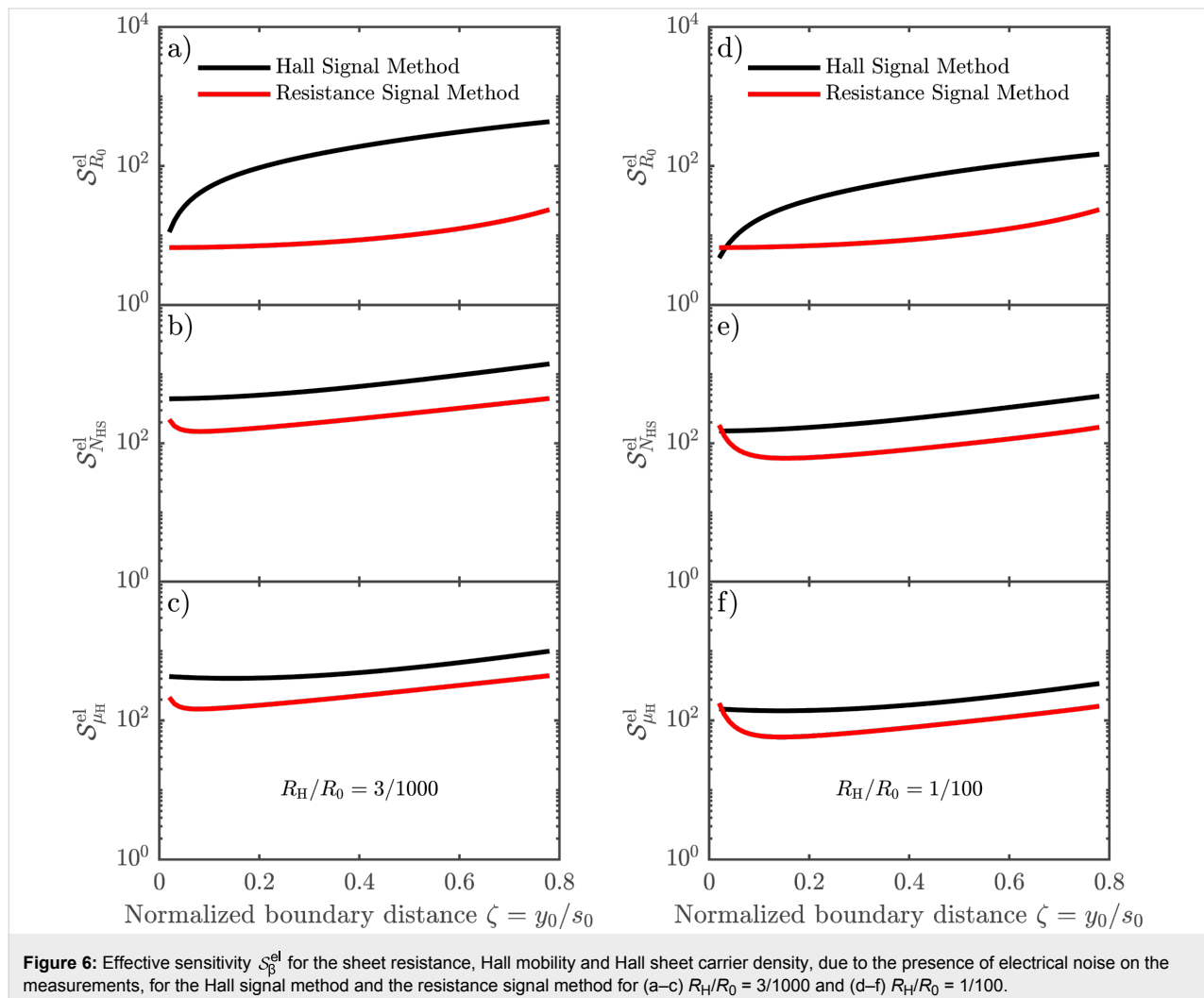
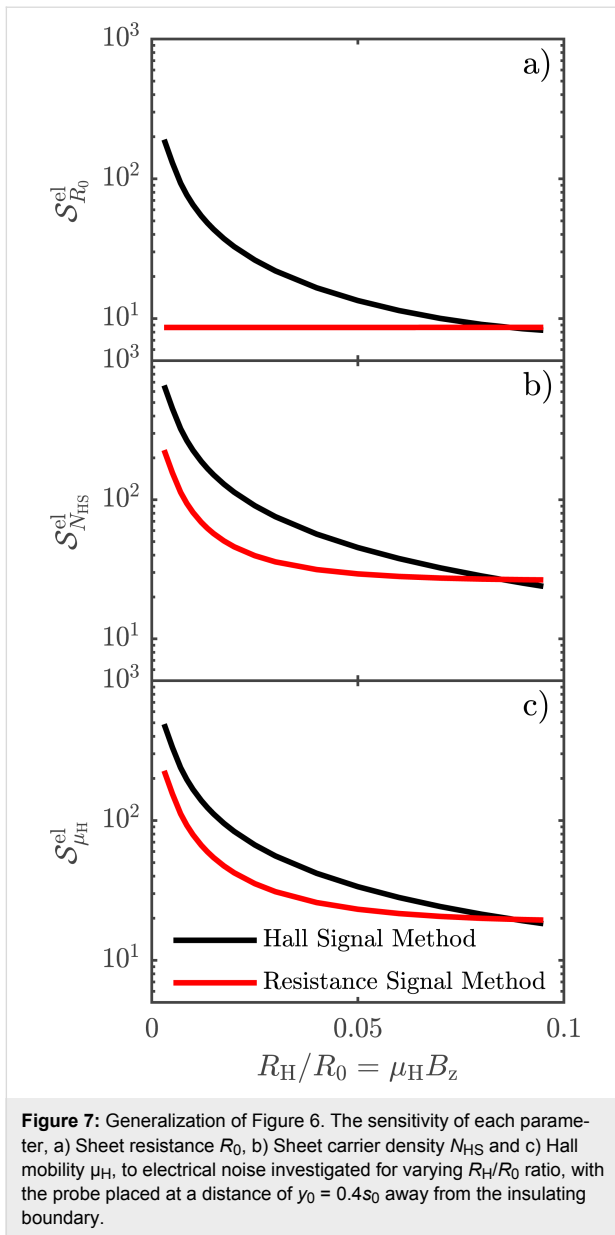


Figure 6: Effective sensitivity S_{β}^{el} for the sheet resistance, Hall mobility and Hall sheet carrier density, due to the presence of electrical noise on the measurements, for the Hall signal method and the resistance signal method for (a–c) $R_H/R_0 = 3/1000$ and (d–f) $R_H/R_0 = 1/100$.



R_H/R_0 ratio. This makes sense, since the magnitude of the Hall signal $\Delta R_{BB'}$ compared to the resistance signal R_m increases with the ratio R_H/R_0 . Now consider the parameters as extracted from the resistance signal method, indicated by the red lines in Figure 7a–c. μ_H and N_{HS} display a similar behaviour as their counterparts in the Hall signal method, although with considerably lower magnitude errors, for the same reason as we have outlined previously. The error on R_0 for the resistance signal method (Figure 7a) displays a behaviour radically different from the others. The reason is that R_0 for the resistance signal method is determined completely without the influence of the Hall signal. Thus, a higher magnitude Hall signal will not result in a reduction of the uncertainty of R_0 . Instead, we see that the error of R_0 is almost constant.

In a real measurement, both position errors and electrical noise are present, and thus the total relative standard deviation of β is

$$\sigma_{\beta}^{\text{rel,tot}} = \sqrt{\left(\sigma_{\beta}^{\text{pos}} \frac{\sigma_{\text{pos}}}{s_0}\right)^2 + \left(\sigma_{\beta}^{\text{el}} \frac{\sigma_v}{IR_0}\right)^2}, \quad (14)$$

where either the first or the second term is dominant depending on the measurement conditions.

Experimental

Measurements were performed using a microHall-A300 tool from CAPRES A/S and an M7PP with an electrode pitch of 10 μm . The M7PP used consisted of nickel-coated poly-silicon cantilever electrodes extending from the edge of a silicon die. A magnetic field with the flux density $B_z = 600$ mT was applied perpendicular to a boron-doped (10^{15} cm^{-2}) shallow-junction Si sample. The probe was placed nominally 4 μm from the insulating boundary during measurements, i.e., $y_0/s_0 = 0.2$. A total of 150 engages was performed parallel to the insulating boundary, keeping the distance between the probe and insulating boundary constant. At each point, 75 configurations using A, A', B and B' configurations were measured; 25 for each of the sub-probes 1357, 1234 and 4567. The different parameters were then extracted using both the resistance signal method and the Hall signal method. The mean extracted values, as well as the standard deviations for each parameter are shown in Table 1.

Table 1: Mean values and standard deviations for the sheet resistance, Hall sheet carrier density and Hall mobility. The measurements were performed under 600 mT flux density and extracted using the resistance signal method and the Hall signal method.

Method	$R_0 \pm \Delta R_0$ Ω	$N_{HS} \pm \Delta N_{HS}$ 10^{14} cm^{-2}	$\mu_H \pm \Delta \mu_H$ $\text{cm}^2/(\text{Vs})$
Hall signal	284 ± 10	3.99 ± 0.34	56.8 ± 3.0
resistance signal	284 ± 2	3.95 ± 0.19	56.0 ± 2.4

Table 1 shows that the standard deviations for the resistance signal method are all lower than the corresponding standard deviations found for the Hall signal method. Based on the discussion about the sensitivities to both position errors and electrical noise, this meets the expectations. When a nominal distance to the edge of 4 μm is used during measurements, the resistance signal method should be the most accurate in all cases, according to Figure 5. Furthermore, it is observed that the largest relative deviations are found on the sheet carrier densities and the smallest on the sheet resistances, for both methods. This is also in line with our expectations. Finally, we find that the measurement results correspond to the case where the error is dominated by electrical noise.

Conclusion

In this paper, we have presented a variable probe pitch method well-suited for characterization purposes in the development of nanoelectronic materials. We have compared two different analysis methods to obtain the electrical parameters R_0 , μ_H and N_{HS} from MHE measurement data. We have shown that the resistance signal method is more precise when measuring close to the insulating boundary of a sample, whereas the precision of the Hall signal method is better farther away from such a boundary, when static position errors are present. Furthermore, we have calculated the sensitivity of each method to electrical noise, and the resistance signal method proved superior. Finally, we presented MHE measurements on a B-doped Si ultra shallow junction and the experimental results confirmed the theoretical conclusions, since the standard deviations on the parameters were smaller for the resistance signal method, compared to those found for the Hall signal method.

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