



## Supporting Information

for

### **A multi-resistance wide-range calibration sample for conductive probe atomic force microscopy measurements**

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## Additional experimental information

## **S1 – Instrument Calibration**

The DVM Keysight 3458A has an inherent accuracy of few ppm for DC voltage, resistance, and current measurements, which makes it an extremely valuable asset in metrology labs. Both the DVM and the Femto amplifier were calibrated at the French National Metrology Institute (LNE), following the highest standards in metrology (see for example the Key Comparison Data Base of the BIPM: <https://www.bipm.org/kcdb/cmc/quick-search>). The custom-built WCDM device was calibrated in-house using discreet resistances, yielding an uncertainty of 1% for resistances in the range between 100  $\Omega$  and 10<sup>9</sup>  $\Omega$ , and 10%–20% for resistances in the range between 10<sup>10</sup>  $\Omega$  and 10<sup>12</sup>  $\Omega$ . It is worth highlighting that, to our knowledge, there are no readily existing calibrated devices for resistance measurements in C-AFM.

## **S2 – Resistance Correction of the Connection Lines**

To determine the resistance of the connection line segments, we proceeded as follows: We performed four-wire measurements between the intermediate gold pads (300  $\mu\text{m} \times 470 \mu\text{m}$ ) and the ground for the first three arms (100  $\Omega$ , 1 k $\Omega$ , and 10 k $\Omega$ ). We calculated the resistivity ( $\rho = (31.4 \pm 0.4) \cdot 10^{-9} \Omega \cdot \text{m}$ ) using the measured resistance values and dimensions (width and thickness) of the lines. Then, we measured the dimensions of the lines between the intermediate gold pads and the electrodes. Based on the calculated resistivity value and the line dimensions, we calculated their resistance values to make the appropriate corrections.

## **S3 – Measurement Protocol for Reference Values in Table 1**

We collected 100 measurement data for each resistance value ranging from 100  $\Omega$  to 1 G $\Omega$  using the high-precision DVM. This leads to standard deviations not exceeding 4 parts in 10<sup>5</sup>. Moreover, we measured a single  $I$ - $V$  curve for each resistance in the range between 1 G $\Omega$  and 100 G $\Omega$  by sweeping the voltage between -1 V and +1 V with steps of 50 mV. This leads to a standard deviation on the slope of less than 8 parts in 10<sup>5</sup>. These standard deviations reflect the measurement noise. In metrology, we consider this uncertainty as a type-A standard uncertainty (Joint Committee for Guides in Metrology - JCGM. Evaluation of Measurement Data — Guide to the Expression of Uncertainty in Measurement. JCGM 100 2008. <https://www.bipm.org/en/publications/guides/gum.html>).

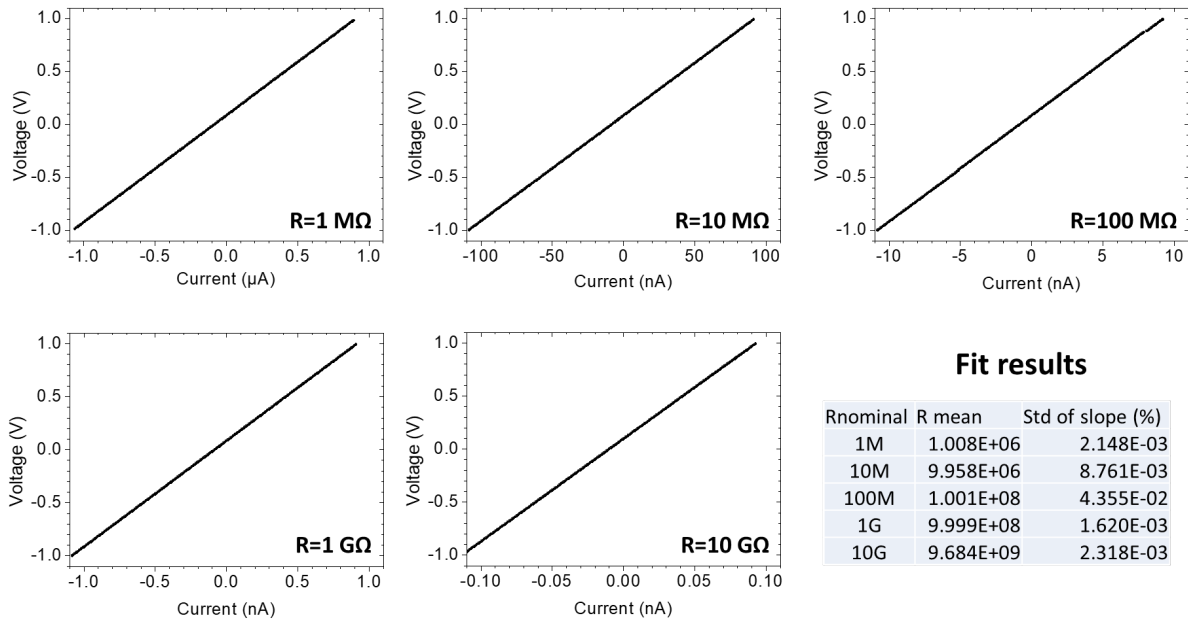
## **S4 – Uncertainty Components (Sample Temperature and Voltage Effect)**

The uncertainty components originating from the sample's temperature and voltage effects were estimated from the temperature coefficient and the voltage effect coefficient given by the manufacturers. In fact, voltage effects correspond to power effects, that is, self-heating of the resistors, generally correlated to the temperature coefficient of that resistor. The temperature coefficient ranges from 10<sup>-4</sup>/K in relative value for 100  $\Omega$  up to 2·10<sup>-3</sup>/K for 100 G $\Omega$ . The voltage coefficient ranges from 5·10<sup>-4</sup>/V for 100  $\Omega$  up to 2·10<sup>-3</sup>/V for 100 G $\Omega$ . A rectangular distribution was considered in both cases. The uncertainty component corresponding to the calibration of the current amplifier gain is mainly dominated by the calibration uncertainty of the resistance standards used to calibrate the gain, that is, three resistances of 1 G $\Omega$ , 10 G $\Omega$ , and 100 G $\Omega$ , with a calibration uncertainty of 2.6 parts in 10<sup>4</sup> (one standard deviation).

## **S5 – $I$ - $V$ Curves Analysis for Resistance Assessment**

$I$ - $V$  curves were analyzed with a custom-made MATLAB-based analysis software to extract resistance measurements from the slope of  $I$ - $V$  curves using a regression model. For each calculated mean value,

the value of  $R^2$  (coefficient of determination) was equal to 1. Figure S1 shows the  $I$ - $V$  curves for nominal resistances values of 1 M $\Omega$ , 10 M $\Omega$ , 100 M $\Omega$ , 1 G $\Omega$ , and 10 G $\Omega$ .



**Figure S1:** Representative examples of the  $I$ - $V$  curves measured on the different resistance pads. The last panel shows the fit results to determine the resistance values from the slopes of the  $I$ - $V$  curves.