

Supporting Information

for

Calculation of the effect of tip geometry on noncontact atomic force microscopy using a qPlus sensor

Julian Stirling*¹ and Gordon A. Shaw²

Address: ¹School of Physics and Astronomy, The University of Nottingham, University Park, Nottingham, NG7 2RD, United Kingdom and ²Physical Measurement Laboratory, National Institute of Standards and Technology, Gaithersburg, Maryland 20899

Email: Julian Stirling* - ppxjs1@nottingham.ac.uk

* Corresponding author

Further details of the presented theoretical model

Appendix A

The boundary conditions in Equations 6–9 allow us to form four simultaneous equations for the factors $b_{1..4}$ of $\Phi_i(x)$ from Equation 4.

$$b_1 + b_3 = 0 \quad (36)$$

$$b_2 + b_4 = 0 \quad (37)$$

$$b_1 \left(-\cos(\beta_i L) + \frac{J\beta_i^2}{\gamma_i} \sin(\beta_i L) \right) + b_2 \left(-\sin(\beta_i L) - \frac{J\beta_i^2}{\gamma_i} \cos(\beta_i L) \right) \\ + b_3 \left(\cosh(\beta_i L) - \frac{J\beta_i^2}{\gamma_i} \sinh(\beta_i L) \right) + b_4 \left(\sinh(\beta_i L) - \frac{J\beta_i^2}{\gamma_i} \cosh(\beta_i L) \right) = 0 \quad (38)$$

$$b_1 (\gamma_i \sin(\beta_i L) + \cos(\beta_i L)) + b_2 (-\gamma_i \cos(\beta_i L) + \sin(\beta_i L)) \\ + b_3 (\gamma_i \sinh(\beta_i L) + \cosh(\beta_i L)) + b_4 (\gamma_i \cosh(\beta_i L) + \sinh(\beta_i L)) = 0 \quad (39)$$

where γ_i is a dimensionless parameter defined as

$$\gamma_i = \frac{EI\beta_i^3}{m_{\text{tip}}\omega_i^2}. \quad (40)$$

Writing Equations 36, 37, 38, and 39 as a matrix equation in the form

$$\underline{\underline{D}} \begin{pmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (41)$$

it becomes clear that if $\det(\underline{\underline{D}}) \neq 0$, then the solution would trivially be $b_{1..4} = 0$, a stationary beam.

Hence, $\det(\underline{\underline{D}}) = 0$, giving the following condition for β_i :

$$1 + m^* \beta_i^4 J L^2 - \left(1 + m^* \beta_i^4 J L^2 \right) \cos(\beta_i L) \cosh(\beta_i L) \\ + m^* \beta_i L \left[(1 - J\beta_i^2) \cos(\beta_i L) \sinh(\beta_i L) - (1 + J\beta_i) \cosh(\beta_i L) \sin(\beta_i L) \right] = 0 \quad (42)$$

using

$$\gamma_i = \frac{\rho A}{\beta_i m_{\text{tip}}} = \frac{1}{\beta_i L m^*}, \quad (43)$$

from Equations 5 and 40, where m^* is the ratio of the tip mass to the mass of the tine. Equation 42 can be numerically solved simply and quickly by using the Newton-Raphson method.

Appendix B

Equation 12 can be expanded to give

$$W = \frac{EI}{2} \left[\sum_{i=1}^{\infty} \mathcal{T}_i^2(t) \int_0^L \left(\frac{d^2 \Phi_i(x)}{dx^2} \right)^2 dx + \sum_{i=1}^{\infty} \sum_{k=1, k \neq i}^{\infty} \mathcal{T}_i(t) \mathcal{T}_k(t) \int_0^L \frac{d^2 \Phi_i(x)}{dx^2} \frac{d^2 \Phi_k(x)}{dx^2} dx \right] \quad (44)$$

Butt and Jaschke [1] use

$$\frac{d^4 \Phi_i(x)}{dx^4} = \beta_i^4 \Phi_i(x) \quad (45)$$

(which is clearly still true for our boundary conditions from the general form of Φ given in Equation 4) to show that the integral with mixed ($\Phi_i(x)$ and $\Phi_k(x)$) second derivatives can be written as

$$\int_0^L \frac{d^2 \Phi_i(x)}{dx^2} \frac{d^2 \Phi_k(x)}{dx^2} dx = \frac{1}{\beta_i^4 - \beta_k^4} \left[\beta_i^4 \frac{d^2 \Phi_k(x)}{dx^2} \frac{d \Phi_i(x)}{dx} - \beta_i^4 \frac{d^3 \Phi_k(x)}{dx^3} \Phi_i(x) - \beta_k^4 \frac{d^2 \Phi_i(x)}{dx^2} \frac{d \Phi_k(x)}{dx} + \beta_k^4 \frac{d^3 \Phi_i(x)}{dx^3} \Phi_k(x) \right]_0^L. \quad (46)$$

If we combine Equations 40 and 43 to give

$$\beta_i^4 L m^* = \frac{m_{\text{tip}} \omega_i^2}{EI} \quad (47)$$

then we can rewrite boundary conditions Equations 8 and 9 as

$$\frac{\partial^2 \Phi_i(L)}{\partial x^2} = \beta_i^4 J L m^* \frac{\partial \Phi_i(L)}{\partial x} \quad (48)$$

$$\frac{\partial^3 \Phi_i(L)}{\partial x^3} = -\beta_i^4 L m^* \Phi_i(L). \quad (49)$$

From these conditions it becomes clear that the first and third terms in the square brackets of Equation 46 cancel, as do the second and fourth. Thus,

$$\int_0^L \frac{d^2 \Phi_i(x)}{dx^2} \frac{d^2 \Phi_k(x)}{dx^2} dx = 0, \quad (50)$$

and

$$W = \frac{EI}{2} \sum_{i=1}^{\infty} \mathcal{F}_i^2(t) \int_0^L \left(\frac{\partial^2 \Phi_i(x)}{\partial x^2} \right)^2 dx. \quad (51)$$

Appendix C

To solve Λ_i we first integrate by parts twice to give

$$\Lambda_i = \left[\frac{d\Phi_i(x)}{dx} \frac{d^2 \Phi_i}{dx^2} - \Phi_i(x) \frac{d^3 \Phi_i(x)}{dx^3} \right]_0^L + \int_0^L \Phi_i(x) \frac{d^4 \Phi_i(x)}{dx^4} dx. \quad (52)$$

The square brackets can be evaluated using boundary conditions from Equations 6, 7, 48, and 49.

Furthermore, with Equation 45 the integral can be written in terms of $\Phi_i(x)$ only:

$$\Lambda_i = \beta_i^4 L J m^* \left(\frac{d\Phi_i(L)}{dx} \right)^2 + \beta_i^4 L m^* \Phi_i^2(L) + \beta_i^4 \int_0^L \Phi_i(x)^2 dx. \quad (53)$$

The integral can be solved by substituting in $\zeta = x/L$, and writing $\beta_i L$ as α_i ,

$$\begin{aligned}
\int_0^L \Phi_i^2 dx &= L \int_0^1 \left\{ \left[\sin(\alpha_i) + \sinh(\alpha_i) - \frac{J\beta_i^2}{\gamma_i} (-\cos(\alpha_i) + \cosh(\alpha_i)) \right] \right. \\
&\quad \times (\cos(\alpha_i \zeta) - \cosh(\alpha_i \zeta)) \\
&\quad - \left[\cos(\alpha_i) + \cosh(\alpha_i) - \frac{J\beta_i^2}{\gamma_i} (\sin(\alpha_i) + \sinh(\alpha_i)) \right] \\
&\quad \left. \times (\sin(\alpha_i \zeta) - \sinh(\alpha_i \zeta)) \right\}^2 d\zeta \tag{54} \\
&= L \left(\sin(\alpha_i) + \sinh(\alpha_i) \right)^2 \\
&\quad + \frac{3L}{\alpha_i} \left(1 + \cos(\alpha_i) \cosh(\alpha_i) \right) \\
&\quad \times \left(-\cosh(\alpha_i) \sin(\alpha_i) + \cos(\alpha_i) \sinh(\alpha_i) \right) \\
&\quad - \frac{J\beta_i^2}{\gamma_i} L \left\{ \frac{1}{\alpha_i} \left[-4 + \cos(2\alpha_i) + \left(1 + 2\cos(2\alpha_i) \right) \cosh(2\alpha_i) \right] \right. \\
&\quad \left. - 2(\cos(\alpha_i) - \cosh(\alpha_i))(\sin(\alpha_i) + \sinh(\alpha_i)) \right\} \\
&\quad + \frac{J^2\beta_i^4}{\gamma_i^2} L \left[\left(\cos(\alpha_i) - \cosh(\alpha_i) \right)^2 \right. \\
&\quad + \frac{3}{\alpha_i} \left(-1 + \cos(\alpha_i) \cosh(\alpha_i) \right) \\
&\quad \left. \times \left(\cosh(\alpha_i) \sin(\alpha_i) + \cos(\alpha_i) \sinh(\alpha_i) \right) \right]. \tag{55}
\end{aligned}$$

Returning back to notation without α_i or γ_i and using Equation 42 to replace $(1 + \cos(\beta_i L) \cosh(\beta_i L))$ in the second term, after some manipulation gives

$$\begin{aligned}
&= L \left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 \\
&\quad - 3Lm^* \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right)^2 \\
&\quad - \beta_i^2 Jm^* L \left[-\frac{5}{2} + \cos(2\beta_i L) + \cosh(2\beta_i L) \right. \\
&\quad + \frac{1}{2} \cos(2\beta_i L) \cosh(2\beta_i L) \\
&\quad - 2\beta_i L \left(\cos(\beta_i L) - \cosh(\beta_i L) \right) \left(\sin(\beta_i L) + \sinh(\beta_i L) \right) \\
&\quad \left. - 3m^* \beta_i L \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \right. \\
&\quad \left. \times \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \right] \\
&\quad + \beta_i^6 J^2 m^{*2} L^3 \left[\left(\cos(\beta_i L) - \cosh(\beta_i L) \right)^2 \right] \\
&\quad + 3\beta_i^5 J^2 m^{*2} L^2 \left[\left(-1 + \cos(\beta_i L) \cosh(\beta_i L) \right) \right. \\
&\quad \left. \times \left(\cosh(\beta_i L) \sin(\beta_i L) + \cos(\beta_i L) \sinh(\beta_i L) \right) \right]. \tag{56}
\end{aligned}$$

Using Equation 42 again, this time to replace $\beta_i^3 J m^* L (\cosh(\beta_i L) \sin(\beta_i L) + \cos(\beta_i L) \sinh(\beta_i L))$ in the final term, and rearranging will give

$$\begin{aligned}
\int_0^L \Phi_i^2 dx = & L \left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 \\
& - 3Lm^* \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right)^2 \\
& - \beta_i^2 J m^* L \left[\sin^2(\beta_i L) \sinh^2(\beta_i L) \right. \\
& - 2\beta_i L \left(\cos(\beta_i L) - \cosh(\beta_i L) \right) \times \left(\sin(\beta_i L) + \sinh(\beta_i L) \right) \\
& - 6m^* \beta_i L \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \\
& \times \left. \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \right] \\
& + \beta_i^6 J^2 m^{*2} L^3 \left[\left(\cos(\beta_i L) - \cosh(\beta_i L) \right)^2 \right. \\
& \left. - 3m^* \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right)^2 \right]. \tag{57}
\end{aligned}$$

It can be shown simply that

$$\left(\frac{d\Phi_i(L)}{dx} \right)^2 = 4\beta_i^2 \sin^2(\beta_i L) \sinh^2(\beta_i L), \tag{58}$$

and that

$$\begin{aligned}
\Phi_i^2(L) = & 4 \left[\left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right)^2 \right. \\
& - 2\beta_i^3 J m^* L \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \\
& \times \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \\
& \left. + \beta_i^6 J^2 m^{*2} L^2 \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right)^2 \right]. \tag{59}
\end{aligned}$$

Note that this form of $\Phi_i^2(L)$ appears in Equation 57, allowing us to reduce it to

$$\begin{aligned}
\int_0^L \Phi_i^2 dx = & L \left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 - \frac{3Lm^*}{4} \Phi_i^2(L) \\
& - \beta_i^2 J m^* L \left[\sin^2(\beta_i L) \sinh^2(\beta_i L) \right. \\
& \left. - 2\beta_i L \left(\cos(\beta_i L) - \cosh(\beta_i L) \right) \left(\sin(\beta_i L) + \sinh(\beta_i L) \right) \right] \\
& + \beta_i^6 J^2 m^{*2} L^3 \left(\cos(\beta_i L) - \cosh(\beta_i L) \right)^2.
\end{aligned} \tag{60}$$

Combining Equations 58, 59, and 60 after some manipulation gives

$$\begin{aligned}
\Lambda_i = & \frac{\beta_i^4 L m^*}{4} \Phi_i^2(L) + \beta_i^4 L \left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 \\
& - \beta_i^6 J m^* L \left[-3 \sin^2(\beta_i L) \sinh^2(\beta_i L) \right. \\
& \left. - 2\beta_i L \left(\cos(\beta_i L) - \cosh(\beta_i L) \right) \left(\sin(\beta_i L) + \sinh(\beta_i L) \right) \right] \\
& + \beta_i^{10} J^2 m^{*2} L^3 \left(\cos(\beta_i L) - \cosh(\beta_i L) \right)^2.
\end{aligned} \tag{61}$$

Which for simplicity, can be written as

$$\Lambda_i = \frac{\beta_i^4 L m^*}{4} \Phi_i^2(L) + \beta_i^4 L \left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 + \beta_i^6 J m^* L f(m^*, J), \tag{62}$$

where

$$\begin{aligned}
f(m^*, J) = & 3 \sin^2(\beta_i L) \sinh^2(\beta_i L) \\
& + 2\beta_i L \left(\cos(\beta_i L) - \cosh(\beta_i L) \right) \left(\sin(\beta_i L) + \sinh(\beta_i L) \right) \\
& + \beta_i^4 J m^* L^2 \left(\cos(\beta_i L) - \cosh(\beta_i L) \right)^2.
\end{aligned} \tag{63}$$

By substituting Equation 42 into Equation 59 and rearranging we get

$$\begin{aligned}
\Phi_i^2(L) = & 4 \left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 \\
& - 8\beta_i L m^* \sin(\beta_i L) \sinh(\beta_i L) \\
& \times \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \\
& + 8\beta_i^3 L J m^* \left[- \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \right. \\
& \times \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \\
& - \sin(\beta_i L) \sinh(\beta_i L) \left(\cosh(\beta_i L) \sin(\beta_i L) + \cos(\beta_i L) \sinh(\beta_i L) \right) \\
& \left. + \beta_i L m^* \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \sin(\beta_i L) \sinh(\beta_i L) \right] \\
& + 4\beta_i^6 L^2 J^2 m^{*2} \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right)^2. \tag{64}
\end{aligned}$$

Initially this form appears to be more complicated. However, as will be demonstrated, because it contains the boundary conditions it produces a final result that is more physically understandable.

For simplicity it can be written as

$$= 4 \left[\left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 - \beta_i L m^* \left(2g + \beta_i^2 J h(m^*, J) \right) \right], \tag{65}$$

where

$$g = \sin(\beta_i L) \sinh(\beta_i L) \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \tag{66}$$

and

$$\begin{aligned}
h(m^*, J) = & 2 \left[- \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \right. \\
& \times \left(\cosh(\beta_i L) \sin(\beta_i L) - \cos(\beta_i L) \sinh(\beta_i L) \right) \\
& - \sin(\beta_i L) \sinh(\beta_i L) \left(\cosh(\beta_i L) \sin(\beta_i L) + \cos(\beta_i L) \sinh(\beta_i L) \right) \\
& + \beta_i L m^* \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right) \sin(\beta_i L) \sinh(\beta_i L) \left. \right] \\
& + \beta_i^3 L J m^* \left(1 - \cos(\beta_i L) \cosh(\beta_i L) \right)^2
\end{aligned} \tag{67}$$

Thus, finally we can write

$$\begin{aligned}
\frac{\Lambda_i L^3}{\Phi_i^2(L)} = & \frac{\beta_i^4 L^4}{4} \left(m^* \right. \\
& \left. + \frac{\left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 + \beta_i^2 J m^* f(m^*, J)}{\left(\sin(\beta_i L) + \sinh(\beta_i L) \right)^2 - \beta_i L m^* \left(2g + \beta_i^2 J h(m^*, J) \right)} \right).
\end{aligned} \tag{68}$$

It is clear that in the case of no tip, $m^* = 0$, this reduces to just $\frac{\beta_i^4 L^4}{4}$. Inserting this into Equation 16 yields a result consistent with Melcher et al. [2]. Further consistency with the literature can be shown in the case of the point mass, where $J = 0$ but $m^* \neq 0$. Inserting Equation 68 into Equation 16 with these conditions, agrees with the results of Lozano et al. [3].

A final test of the accuracy of this equation can be done by considering equipartition theorem with Hooke's law in terms of the static spring constant:

$$\frac{1}{2} k_B T = \frac{1}{2} k_{\text{stat}} \sum_{i=1}^{\infty} \langle Z_i^2(L) \rangle \tag{69}$$

and inserting Equation 15 we get

$$\sum_{i=1}^{\infty} \frac{L^3 \Lambda_i}{\Phi_i^2(L)} = 3. \tag{70}$$

Using the same model qPlus sensor as described above, this has been plotted in Figure 1, for $i = 1..8$ showing excellent agreement with theory, and faster convergence for larger tips.

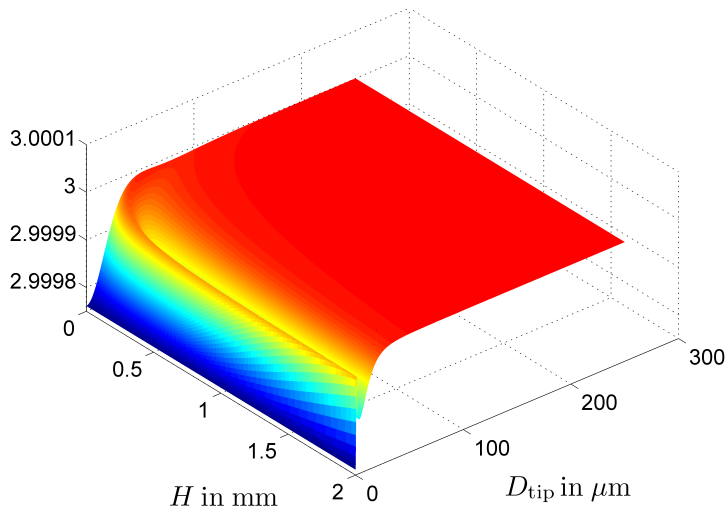


Figure S 1: Agreement with $\lim_{N \rightarrow \infty} \sum_{i=1}^N \frac{L^3 \Lambda_i}{\Phi_i^2(L)} = 3$, plotted for $N = 8$ roots to show that the equation is consistent with equipartition theorem. Where H is the length and D_{tip} is the diameter of a cylindrical tip.

References

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